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FLOOD IMPACT ASSESSMENT AND CONCEPT SITE STORMWATER DRAINAGE PLAN



35 EDNA STREET, LILYFIELD

Prepared by:

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Reviewed by:

Stephen Fryer Senior Civil Engineer

Job Number: 09447 Revision 3

Date: 1st October, 2009

1.0 INTRODUCTION

Sydney Water Corporation (SWC) is proposing to subdivide Lot 1 in DP343175 (known as 35 Edna Street, Lilyfield). The site is bordered by Piper Street (north), Edna Street (west) and White Street (east). It occupies a total area of 2178m² and slopes in the easterly direction at approximately 7% from west to east.

Northrop Consulting Engineers has been engaged by Sydney Water Corporation to:

- a) Undertake a Flood Impact Assessment for the subject site, and
- b) Prepare a Concept Site Stormwater Management Plan for the proposed subdivision.

The following report has been prepared in response to this – in order to support Development Application for Subdivision of the lot.

The proposed subdivision will provide 5 lots. Lots 1-4 will be residential lots located on the northern side of the site (refer to Appendix 5, drawing number 09447-DA01). The residential lots will occupy a total area of 1270m². The remaining southern portion of the site (910m²) will be Lot 5 and remain under SWC ownership (and use).

2.0 BACKGROUND DRAINAGE INFORMATION

Northrop has referred to the following information as background to stormwater runoff affecting the subject site:

- 'Preliminary Stormwater Investigation", undertaken by Patterson Britton & Partners (dated December 2005) concluded the site was subjected to overland flow through a low point located at Edna Street.
- Orthophoto map (Leichhardt U0945-61) the contours indicate a local depression that may concentrate flow through the site.
- Detailed site survey plan prepared by Degotardi, Smith and Partners (reference number 30408A01.DWG). This shows detailed levels and a drainage pipe passing through the southern part of the site.

This report has been prepared to support Development Application for Subdivision. In particular the following assessments have been made for stormwater components:

- 1. Identify and analyse the stormwater drainage system in vicinity of the site.
- 2. Determine 100-year ARI flows and flow paths affecting the site.
- 3. Prepare a Concept Site Stormwater Management Plan (incorporating on-site stormwater detention as required).

3.0 FLOOD IMPACT ASSESSMENT

3.1 Hydrological and hydraulic analysis

A localised depression exists on the eastern side of Edna Street – adjacent to the south-west corner of the subject site. The nature of this depression leads to the potential for overland flow to enter the southern portion of the site in times of blockage or overflow of the street drainage system. The "Catchment Plan" (refer to Appendix 1- 09447-SK01) indicates the catchment areas contributing runoff to the Edna Street low point.

The "Catchment Plan" shows two (2) sub-catchments that have been analysed to determine flow to the Edna Street low point in the 100 year Average Recurrence Interval (ARI) storm event.

- Sub-catchment 1 Catchment contributing flow direct from Edna Street.
- Sub-catchment 2 Catchment contributing to the Piper Street drainage system. This recognises the potential for overflow from
 - system. This recognises the potential for overflow from the piped system to contribute to the Edna Street low point.

The Rational Method was used to calculate Sub-catchment flows. The rainfall intensity values used were as stated in Leichhardt Councils Draft Stormwater Requirements – Supplement 3.

The following table summarises the results of the simplified analysis of Subcatchment flows.

Sub-catchment	Area	%			
	(m²)	impervious	Total catchment	Pipe	Overland
1 - Piper Street	9655	80	0.60	0.14 ²	0.46
2 - Edna Street	12130	80	0.75	0.00 ³	0.75
		Total 100 yea	ar ARI flow		1.21

Note: 1. Flow to Edna Street low point.

2. Allowance for pipe flow in Piper Street has been made to determine quantity of overflow to Edna Street – based on 50% blockage.

3. No allowance for pipe inflow has been made for Edna Street catchment – 100% blockage required by Council for overland flow assessment.

3.2 Overland flow path analysis

Section 3.1 assesses the local stormwater runoff contributing to the low point in Edna Street. A total 100-year ARI flow of 1.21m³/s has been determined to potentially be conveyed through the site. This is based on full (100%) pipe blockage in Edna Street (in accordance with Council requirements).

This section of the report describes the nature by which overland flow would be managed under (a) pre-developed and (b) post-developed scenarios.

a)Pre-development overland flow

In the event that the stormwater pipe at the Edna Street low point is blocked, overland flow would build up over the kerb, footpath and then an additional 250mm depth (over an existing retaining wall at the boundary) before entering the site at the western site boundary (refer to Figure 1).



Figure 1: View from Edna Street along western site boundary showing kerb inlet pit at the depression.

Upon entering the site, flow is directed along the western side of the building, then across the northern frontage. Site inspection indicates that the overland flow most likely discharges to White Street via a stormwater drainage structure on the corner of Piper and White Street refer to Figure 2.



Figure 2: Left shows ponding of overland flow on the north-east point of site; right shows the stormwater drainage structure on the corner of Piper and White Street.

b) Post-development overland flow

Proposed site planning

All buildings on the site are proposed to be demolished to enable four (4) residential lots to be established on the northern portion of the proposed subdivision. As a result, the existing site overland flow path is proposed to be diverted through proposed Lot 5. This will provide a more direct route to the receiving trunk drainage system (in White Street) and address any effect to the proposed residential properties.

In addition it is recommended that the retaining wall along the Edna Street frontage is adjusted. This is in order to direct overflow from Edna Street to the southern portion of the site (only). In this regard it is proposed to lower the top of the existing retaining wall to footpath level for the portion of wall fronting the southern portion of the site (i.e. southern 15m).

Proposed site levels

The creation of new lots will require the existing site levels to be raised to suit street levels along Edna and Piper Street. This will provide for separate driveway entries for the respective lots. Refer to Appendix 5, drawing number 09447- DA01.

Such site levels could be conditioned as part of a Consent to the Subdivision and activated through subsequent future Development Applications for dwelling houses.

Proposed overland flow calculations

Entering off Edna Street

Calculations have been performed using the broad-crested weir equation to determine the height of water at the location planned for overflow from Edna Street. The calculations indicate the depth of water will be approximately 130mm across the 15.0m length under 100-year ARI storm conditions – refer to Appendix 4.

Conveyed through southern portion (Lot 5)

A HEC-RAS model was developed to model the proposed southern portion of the site (Lot 5) to determine the level of flow in the 100 year ARI flood event. Detailed survey information provided by Degotardi, Smith & Partners was used to develop cross section information. Existing buildings along the south and proposed buildings along the north were entered in as blockouts.

A Manning's "n" roughness value of 0.035 was used for the southern portion of the site.

The results of the overflow calculations indicate the maximum depth to be 150mm. Refer to Appendix 2 for HEC-RAS output/results.

Northrop drawing number 09447-DA02, Appendix 6, provides an overview of the scheme for overland flow management through the proposed development site, including general outcomes of the calculations. It also shows 500mm freeboard protection will be to adjoining floor levels from the calculated 100-year ARI flow through the southern portion (Lot 5).

4.0 CONCEPT SITE STORMWATER MANAGEMENT PLAN

A Concept Site Stormwater Management Plan has been prepared to support the Development Application for Subdivision. The plan indicates proposed measures to manage stormwater runoff and discharge from the proposed residential portion of the subject site.

The concept stormwater management scheme incorporates provisions for On-site Stormwater Detention (OSD) in accordance with Council requirements. Preliminary calculation for OSD are summarised as follows:

Pre-development conditions:

Area = $312m^2$ Impervious area = 50% (actual 90-95%) Time of concentration (t_c) = 5min paved = 11min grassed Note: reduced impervious area reduces actual pre-development runoff.

Post-development conditions:

Area = $312m^2$ Impervious area = 80%(t_c) = 5min paved = 11min grassed

The storage volume for OSD provisions was calculated by comparing the 100 year ARI post-development site discharge with the 5 year ARI pre-development site discharge (in accordance with Council requirements). This was calculated using the DRAINS software program.

The following table provides a summary of the design flows calculated in the model. The post-development flows are based on providing $5m^3$ OSD per lot (based on a maximum site area of $312m^2$). Refer to Appendix 4 for DRAINS input and output values.

ARI	Pre-Development (I/s)	Post-Development (I/s)
5	13	10
10	15	10
20	17	11
100	20	12

A possible layout for stormwater management measures is shown on the Concept Site Stormwater Drainage Plan (drawing number 09447-DA01, Appendix 5). This indicates the general layout for stormwater drainage to discharge to Piper and White Street (including provision for an inter-allotment drainage network to service the south-western lot (Lot 3)).

Such recommendations for OSD and drainage could be conditioned as part of Consent for the Subdivision, and activated upon future Development Application's for residential housing.

5.0 CONCLUSIONS

- There is risk of overland flow from the Edna Street drainage system affecting the subject site. This will be conveyed through the southern (undeveloped) portion of the subdivided lot.
- The following minimum floor levels are recommended for proposed future dwellings on the northern part of the site, refer to Appendix 5.

Lot 1	12.95
Lot 2	9.80
Lot 3	15.65
Lot 4	11.60

This makes an allowance for 500mm freeboard above 100-year ARI flows in the southern portion of the site and suitable levels for driveway access from the street.

• The minimum heights for floor levels and/or bunding are required to contain Edna Street overflow within the southern site corridor and achieve minimum 500mm freeboard to floor levels. This applies to both proposed and existing lots directly adjacent to the corridor. Referring to Appendix 3, the required levels for the existing lots along the southern boundary of the site and the proposed lots will be required as follows;

Position along boundary	100-year ARI flood level (m)	Minimum flood planning	Proposed bund/flood protection level (RL – m	
		level (RL – m)	Existing lots	Proposed lots
West side	13.89	14.39	14.86	15.15
Middle	12.33	12.83	12.83	12.83
East side	10.77	11.27	11.27	11.27

- Overflow from Edna Street will occur via the remaining SWC owned portion of the site. Flow will be directed from the street by lowering the boundary wall to footpath level across the frontage at the southern site portion.
- A Concept Site Stormwater Management Plan for the site has been prepared to comply with Leichhardt Council requirements for stormwater. This incorporates grassed basins for On-site Stormwater Detention (OSD). The volume of each basin is approximately 10m³ per lot; required volume is doubled as it is in a landscaped area as per Leichhardt Council guidelines discharging to Piper and White Street. Plan shows nominal locations for rainwater harvesting tanks.
- Buildings along the southern boundary will require bunding for flood protection as shown on Concept Site Stormwater Drainage Plan, Appendix 5 (drawing number 09447-DA01).
- The above recommended levels and drainage management measures could be conditioned as part of the Subdivision Development Application approval and activated as part of the future Development Applications for the dwelling houses.

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APPENDIX 1 -CATCHMENT PLAN - 09447 SK01



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APPENDIX 2 – WEIR FLOW CALCULATION

PROJECT: SWC PIPER ST, MLYFIELS JOB No: 09447



PAGE No: DESIGNED:

DATE: 09.07.09

Sydney Newcastle Canberra Wollongong Northrop Engineers Pty Ltd ABN 82 064 775 088

· NEIR FLOW CALC. (ALONG EDNA STREET) QTOT = 1.21 m3/5 Q = (d . A. J. 2g. Th PROPOSED SITE 15M SOUTHERN BOUNDARY SITE h t BOUNDARY Cd = 0-41 A. = 1.95 m2 Tu = 0.13 m V OK < Qrot = 1.21 m3/5 Q = 1-28 m3/5

Civil Hydraulic Mechanical Structural Electrical Environmental Civil Hydraulic Electrical Environmental Civil Hydraulic Mechanical Structural Electrical Environmental Civil Hydraulic Mechanical Structural Electrical Environmental Civil Hydraulic Mechanical Structural

APPENDIX 3 – HEC-RAS



None of the XS's are Geo-Referenced (Geo-Ref user entered XS+Geo-Ref interpolated XS+Non Geo-Ref user entered XS+Non Geo-Ref interpolated XS)

Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
			(m3/s)	(m)	(m)	(m)	(m)	(m/m)	(m/s)	(m2)	(m)	
Piper Street	63	PF 1	1.21	13.39	13.64	13.64	13.70	0.025230	1.11	1.09	8.71	1.00
Piper Street	47.5	PF 1	1.21	13.00	13.14	13.14	13.18	0.028273	0.93	1.30	15.00	1.01
Piper Street	32	PF 1	1.21	12.29	12.38	12.38	12.43	0.027690	0.93	1.30	14.99	1.01
Piper Street	16.5	PF 1	1.21	11.25	11.36	11.36	11.40	0.028119	0.93	1.30	15.00	1.01
Piper Street	1	PF 1	1.21	10.62	10.71	10.71	10.75	0.027907	0.93	1.30	14.91	1.01

HEC-RAS Plan: Plan 01 River: Piper Street Reach: Piper Street Profile: PF 1

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APPENDIX 4 – DRAINS INPUT AND OUTPUT DATA





09447 35 Edna Street, Lilyfield DRAINS Layout

09447 53 Edna Street, Lilyfield OSD Calculations Input Data

PIT / NOD Name	E DETAILS Type	Family	Version 9 Size	Ponding Volume	Pressure Change	Surface Fley (m)	Max Pond Depth (m)	Base Inflow	Blocking Factor	x	У	Bolt-down lid	id	Part Full Shock Lo	ss						
				(cu.m)	Coeff. Ku	,	2 op ()	(cu.m/s)						0.1001120							
N52 N55	Node Node					11.41 11.41	L	C)	1673.68 1464.88	-1257.52 -1313.68	3	128 132	<u>}</u>							
DETENTIO	N BASIN DE	TAILS																			
Name	Elev	Surf. Area	Init Vol. (cu.m)	Outlet Type	К	Dia(mm)	Centre RL	Pit Family	Pit Type	X	у	HED	Crest RL	Crest Len	gtid						
Basin2	11.2 11.5 11.51 11.7	2 0.36 5 0.36 L 27 7 27	5 7	J Orifice		100) 11.28			1534.166	-1256.91	L NO			130	J					
		τλμς																			
Name	Pit or	Total	Paved	Grass	gauZ	Paved	Grass	gans	Paved	Grass	Supp	Paved	Grass	gauS	Paved	Grass	gang	Lag Time	Gutter	Gutter	Gutter
	Node	Area	Area	Area	Area	Time	Time	Time	Length	Length	Length	Slope(%)	Slope	Slope	Rough	Rough	Rough	or Factor	Length	Slope	FlowFactor
		(ha)	%	%	%	(min)	(min)	(min)	(m)	(m)	(m)	%	%	%					(m)	%	
Pre-Devel	o N52	0.0312	2 50) 50	() 5	5 11)									(0		
Post-Deve	l Basin2	0.0312	2 80) 20) ()	5 11	. C)									(0		
PIPE DETA	ILS																				
Name	From	То	Length	U/S IL	D/S IL	Slope	Туре	Dia	I.D.	Rough	Pipe Is	No. Pipes	Chg From	At Chg	Chg	RI	Chg	RL	etc		
			(m)	(m)	(m)	(%)		(mm)	(mm)						(m)	(m)	(m)	(m)	(m)		
Pipe38	Basin2	N55	2	2 11.23	11.21	L 1	L uPVC, unde	e 100) 105	0.03	NewFixed	1	Basin2		0						
DETAILS o	f SERVICES (CROSSING F	PIPES																		
Pipe	Chg	Bottom	Height of Servic	e Chg	Bottom	Height of	S Chg	Bottom	Height of S	Setc											
	(m)	Elev (m)	(m)	(m)	Elev (m)	(m)	(m)	Elev (m)	(m)	etc											
CHANNEI	DETAILS																				
Name	From	То	Туре	Length	U/S IL	D/S IL	Slope	Base Widt	Ł.B. Slope	R.B. Slope	Manning	Depth	Roofed								
				(m)	(m)	(m)	(%)	(m)	(1:?)	(1:?)	n	(m)									
OVERFLO	N ROUTE DI	ETAILS																			
Name	From	То	Travel	Spill	Crest	Weir	Cross	Safe Dept	n SafeDepth	Safe	Bed	D/S Area		id							
			Time	Level	Length	Coeff. C	Section	Major Sto	r Minor Stor	DxV	Slope	Contributi	ng								
051	Dealer 2		(min)	(m)	(m)		7. Duna	(m)	(m)	(sq.m/sec)	(%)	%		4.7	7						
OFT	Basinz	N55	1	ı 11./1	. 1	L 1.67	ummy1	0.3	0.3	0.4	• 1	L 0	1	13	/						

09447 53 Edna Street, Lilyfield OSD Calculations 100yr ARI Output Data

PIT / NODE	E DETAILS			Version 8			
Name	Max HGL	Max Pond HGL	Max Surface Flow Arriving (cu.m/s)	Max Pond Volume (cu.m)	Min Freeboar (m)	Overflow d (cu.m/s)	Constraint
N55	11.3	1	()			
SUB-CATCI	HMENT DETA	ILS					
Name	Max	Paved	Grassed	Paved	Grassed	Supp.	Due to Storm
	Flow Q	Max Q	Max Q	Тс	Тс	Тс	
	(cu.m/s)	(cu.m/s)	(cu.m/s)	(min)	(min)	(min)	
Pre-Develo	0.0	2 0.01	1 0.009	95	1	1	0 AR&R 100 year, 25 minutes storm, average 145.1 mm/h, Zone 1
Post-Devel	l 0.02	1 0.01	8 0.004	4 5	1	1	0 AR&R 100 year, 25 minutes storm, average 145.1 mm/h, Zone 1
Storm	Total Rainfa cu.m	II Total Runoff cu.m (Runoff %) 5 12 10 (87 4%)	Impervious Runoff cu.m (Runoff %) 8 60 (95 5%)	Pervious R cu.m (Run 3 51 (72 49	unoff off %) %)		
AR&R 100	13.8	5 12.10 (87.4%) 6 20 11 (01 E%)	8.00 (95.5%) 12 97 (07.2%)	5.51 (72.4) 6 32 (91 10	70) D/)		
AR&R 100	21.5	6 26 19 (93.0%)	13.87 (97.2%)	8 29 (8/ 19	~~) %)		
AR&R 100	33	3 31 22 (93 8%)	21 24 (98 1%)	9 98 (85 69	%)		
AR&R 100	37.7	3 35.53 (94.2%)	24.12 (98.3%)	11.41 (86.4	4%)		
AR&R 100	41.6	5 39.34 (94.5%)	26.67 (98.5%)	12.68 (87.0	0%)		
AR&R 100	59.5	9 56.63 (95.0%)	38.33 (99.0%)	18.30 (87.8	8%)		
AR&R 100	68.4	2 64.81 (94.7%)	44.07 (99.1%)	20.74 (86.6	6%)		
AR&R 100	75.2	5 70.99 (94.3%)	48.51 (99.2%)	22.48 (85.3	3%)		
AR&R 100	85.7	4 80.19 (93.5%)	55.32 (99.3%)	24.87 (82.9	9%)		
AR&R 100	97.4	4 89.93 (92.3%)	62.93 (99.4%)	27.00 (79.2	2%)		
PIPE DETA	ILS						
Namo	Max O	Max V	May 11/S	May D/S	Due to St	orm	

Name	Max Q	Max V (m/s)	Max U/S	Max D/S	Due to Storm
Pipe38	0.012	<u>(</u>	1.4	11.342 11.3	1 AR&R 100 year, 1 hour storm, average 95.5 mm/h, Zone 1
CHANNEL Name	DETAILS Max O	Max V	Chainage	Мах	Due to Storm

···a			0.1.4.1.4.80		200 10 010111
	(cu.m/s)	(m/s)	(m)	HGL (m)	

OVERFLOW ROUTE DETAILS

Name	Max Q U/S	Max Q D/S	Safe Q	Max D	Max DxV	Max Wio	lth Max V	Due to Storm
OF1	0		0	2.969	0	0	0	0

DETENTION	BASIN	
DETENTION	DADIN	DLIAILS

Name	Max WL	MaxVol	Max Q		Max Q	Max Q
			Total		Low Level	High Level
Basin2	11.6	7	4.5	0.012	0.012	0

CONTINUITY CHECK for AR&R 100 year, 25 minutes storm, average 145.1 mm/h, Zone 1

Node	Inflow Outflow			Storage Chan	ge	Difference	
	(cu.m)	(cu.m)		(cu.m)		%	
N52	17.43	3	17.43		0		0
Basin2	18.3	L	18.08	:	0.01		0.1
N55	18.08	3	18.08	:	0		0

09447 53 Edna Street, Lilyfield OSD Calculations 20yr ARI Output Data

PIT / NOD	E DETAILS						Version 8					
Name	Max HGL		Max Pond HGL		Max Surface Flow Arriving (cu.m/s)		Max Ponc Volume (cu.m)	l Min Freeboa (m)	C ard (Overflow [cu.m/s)	Constra	int
N55		11.31			、 <i>, ,</i>	0	, ,	()				
SUB-CATC	HMENT DE	TAILS	David		Crassed		David	Crasso	ч с	Supp	Ducto	Storm
Name			Max O		Max O		To	Tc	ב ג ד	որեր Տորեն	Due to s	storm
	(cum/s)		$(c_1, m/s)$		(cu m/s)		(min)	(min)	(min)		
Pre-Devel	0	0.017	(cuili, s)	0.009	(cum, s)	0.007	()	5	11	,) AR&R 2	0 vear. 25 minutes storm. average 110.2 mm/h. Zone 1
Post-Deve	el	0.018		0.015		0.003	ļ	5	11	() AR&R 2	0 year, 25 minutes storm, average 110.2 mm/h, Zone 1
Outflow V	Total Dair	i otal (atconment (0	.04 im :	pervious + 0.02 p	perviou	is = 0.06 to	otal ha)				
Storm		IIall	rotal Runon	f %)	Impervious Run	1011 \	rervious r	Aunon				
AR&R 20 v		10 74	9 00 (83 8%)	· /0))	6 58 (94 2%)	,	2 42 (64 A	1011 //) 1%)				
AR&R 20	y. Vé	16.9	15.04 (89.0%	, 6)	10.58 (96.3%)		4.46 (75.5	5%)				
AR&R 20	, yŧ	21.54	19.58 (90.9%	, 6)	13.60 (97.1%)		5.98 (79.3	, 3%)				
AR&R 20	, Yŧ	25.36	23.28 (91.8%	<i>.</i> 6)	16.08 (97.5%)		7.21 (81.2	2%)				
AR&R 20	γŧ	28.65	26.47 (92.4%	6)	18.22 (97.8%)		8.25 (82.2	2%)				
AR&R 20	γŧ	31.54	29.25 (92.7%	6)	20.10 (98.0%)		9.15 (82.9	9%)				
AR&R 20	γŧ	44.55	41.61 (93.4%	6)	28.55 (98.6%)		13.06 (83	.7%)				
AR&R 20	ýť	51.39	47.80 (93.0%	6)	33.00 (98.8%)		14.80 (82	.3%)				
PIPE DETA												
Name	Max Q		Max V		Max U/S		Max D/S	Due to S	Storr	n		
	(cu.m/s)		(m/s)		, HGL (m)		, HGL (m)					
Pipe38		0.011		1.3	:	11.337	11.30	7 AR&R 2	0 yea	ar, 25 mii	nutes stor	m, average 110.2 mm/h, Zone 1
CHANNEL	DETAILS								. .			
Name	Max Q		Max V		Chainage		Max	Due to S	Storr	n		
	(cu.m/s)		(m/s)		(m)		HGL (M)					
OVERFLO	W ROUTE D	ETAILS										
Name	Max Q U/	'S	Max Q D/S		Safe Q		Max D	Max Dx	V N	Max Widt	h Max V	Due to Storm
OF1		0		0		2.969	(D	0	(C	0
DETENTIC		ΓΤΛΙΙς										
Name	Max WI		MaxVol		Max O		Max O	Max O				
Nume			WILLKYON		Total		Low Level	High Lev	vel			
Basin2		11.6		2.6		0.011	0.01	1	0			
CONTINU	ITY CHECK f	or AR8	kR 20 year, 25	5 minu	tes storm, avera	ge 110	.2 mm/h, Z	Zone 1				
Node	Inflow		Outflow		Storage Change	2	Difference	е				
N/52	(cu.m)	40.0	(cu.m)	40.0	(cu.m)	-	%	2				
N52 Bacin2		12.9 12 57		12.9		0 01	(U 1				
N55		13.57		13.54		0.01 N	0	- 0				

09447 53 Edna Street, Lilyfield OSD Calculations 10yr ARI Output Data

PIT / NOE	DE DETAILS					Version 8							
Name	Max HGL	Max Por HGL	nd	Max Surface Flow Arrivir (cu.m/s)	e 1g	Max Pond Volume (cu.m)		Min Freeboard (m)		Overflow (cu.m/s)	v (Constraiı	nt
N55	11.3	3			0								
SUB-CAT	CHMENT DE	TAILS											
Name	Max	Paved		Grassed		Paved		Grassed		Supp.	0	Due to St	torm
	Flow Q	Max Q		Max Q		Тс		Тс		Тс			
	(cu.m/s)	(cu.m/s)		(cu.m/s)		(min)		(min)		(min)			
Pre-Deve	elo 0.014	1	0.008		0.006		5		11		0 4	AR&R 10	year, 25 minutes storm, average 95.1 mm/h, Zone 1
Post-Dev	vel 0.015	5	0.013		0.003		5		11		0 A	AR&R 10	year, 25 minutes storm, average 95.1 mm/h, Zone 1
Outflow V	Volumes for	Total Cato	hment	(0.04 imper	vious	+ 0.02 pervi	ou	s = 0.06 to	tal	ha)			
Storm			non woff %	impervious	RUNOI .ff 0/)	Pervious R	un off	011					
AR&R 10			//////////////////////////////////////	5 60 (03 3%	()		211 %1	70)					
AR&R 10	v, 9.50)v∈ 14.7	7 12.84 (81		9.15 (95.3%	-, 6)	3.69 (71 89	,0) %)						
AR&R 10	v 18.67	16.71 (8 ⁻	9.5%)	11.73 (96.7	~, %)	4.98 (76.19	%)						
AR&R 10	v∈ 21.94	19.87 (9	0.6%)	13.86 (97.2	%)	6.02 (78.39	%)						
AR&R 10	y(24.73	3 22.54 (9	1.2%)	15.67 (97.5	%)	6.88 (79.59	, %)						
AR&R 10	,)y∈ 27.18	, 3 24.88 (9	, 1.6%)	17.26 (97.7	, %)	, 7.62 (80.19	, %)						
AR&R 10	∫y∈ 38.13	35.19 (9)	2.3%)	24.38 (98.4	, %)	10.82 (81.0)%)					
AR&R 10	y 44.09	9 40.50 (9	1.9%)	28.25 (98.6	%)	12.25 (79.4	4%)					
PIPE DET.	AILS												
Name	Max Q	Max V		Max U/S		Max D/S		Due to Sto	rm	ı			
Dino20	(cu.m/s)	(m/s)	1 2	HGL (m)	11 225	HGL (III)	0E	AD 9.D 10 V		r 25 minu	itor	storm	$r_{\rm resp} = 0.51 {\rm mm/h}$ Zono 1
ripe30	0.01	L	1.2	-	11.555	11.50	05	ANON 10 y	ca	1, 23 minu	les	storn, a	average 55.1 mm/m, 2011 1
CHANNE	L DETAILS												
Name	Max Q	Max V		Chainage		Max		Due to Sto	rm	า			
	(cu.m/s)	(m/s)		(m)		HGL (m)							
OVERFLO	OW ROUTE DI	ETAILS											
Name	Max Q U/S	S Max Q D)/S	Safe Q		Max D		Max DxV		Max Wid	lth M	∕lax V	Due to Storm
OF1	C)	0		2.969		0		0)	0		0
DETENTIO	ON BASIN DE	TAILS											
Name	Max WL	MaxVol		Max Q		Max Q		Max Q					
				Total		Low Level		High Level					
Basin2	11.56	5	1.7		0.01	0.0	01		0				
CONTINU	JITY CHECK fo	or AR&R 1	0 year	, 25 minutes	storm	, average 9	5.1	. mm/h, Zo	ne	1			
Node	Inflow	Outflow		Storage Cha	ange	Difference							
	(cu.m)	(cu.m)		(cu.m)		%							
N52	10.94	ł	10.94		0	_	0						
Basin2	11.61	L 7	11.57		0.01	Ŭ	1.2						
N55	11.57	/	-11.57		0		υ						

09447 53 Edna Street, Lilyfield OSD Calculations 5yr ARI Output Data

PIT / NOD	DE DETAILS			Version 8			
Name	Max HGL	Max Pond HGL	Max Surface Flow Arriving (cu.m/s)	Max Pond Volume (cu.m)	Min Freeboard (m)	Overflow (cu.m/s)	Constraint
N55	11.3	5		D			
SUB-CATC Name	Max	Paved	Grassed	Paved	Grassed	Sunn	Due to Storm
Name	Flow Q	Max Q	Max Q	Tc	Tc	Зарр. Тс	
	(cu.m/s)	(cu.m/s)	(cu.m/s)	(min)	(min)	(min)	
Pre-Devel	lo 0.012	0.007	0.00	5 5	5 11	C) AR&R 5 year, 25 minutes storm, average 83.6 mm/h, Zone 1
Post-Deve	el 0.013	0.011	0.00	2 5	5 11	C) AR&R 5 year, 25 minutes storm, average 83.6 mm/h, Zone 1
Outflow \	/olumes for .	Total Catchment	t (0.04 impervious	+ 0 02 pervi	0.05 - 0.06 t	otal ha)	
Storm	Total Rain	f Total Runoff	Impervious Runo	ff Pervious R	lunoff	otarnaj	
	cu.m	cu.m (Runoff %	cu.m (Runoff %)	cu.m (Run	off %)		
AR&R 5 y	e; 8.36	6.62 (79.2%)	5.03 (92.5%)	1.59 (54.4	%)		
AR&R 5 y	e; 13.02	2 11.17 (85.8%)	8.06 (95.2%)	3.11 (68.2	%)		
AR&R 5 y	e: 16.5	5 14.54 (88.1%)	10.32 (96.2%)	4.22 (73.0	%)		
AR&R 5 y	e: 19.32	17.26 (89.3%)	12.15 (96.8%)	5.10 (75.4)	%)		
AR&R 5 y	e: 21.74	19.56 (90.0%)	13.72 (97.1%)	5.83 (76.7	%)		
	ei 23.84	21.55 (90.4%)	15.09 (97.4%) 21 17 (08 1%)	6.46 (77.4)	%) %)		
	e: 33.2 e: 38.38	30.27 (91.2%)	21.17 (98.1%) 24 54 (98 4%)	9.10 (78.5 10 26 (76.	70) 4%)		
AR&R 5 v	ei 42.43	38.19 (90.0%)	27.18 (98.5%)	11.02 (74.)	- <i>70)</i> 2%)		
AR&R 5 y	ea 48.67	43.23 (88.8%)	31.23 (98.7%)	12.00 (70.	5%)		
AR&R 5 y	e; 55.88	8 48.55 (86.9%)	35.92 (98.9%)	12.64 (64.	6%)		
PIPE DETA	AILS						
Name	Max Q	Max V	Max U/S	Max D/S	Due to Sto	rm	
Dino29	(cu.m/s)	(m/s)	HGL (m)	HGL (m)		ar 25 minu	itas starm avaraga 82.6 mm/h Zana 1
ырезо	0.01	. 1.2	11.55	2 11.304	FARAR 5 YE	di, 25 mmu	ites storm, average 85.0 mm/n, zone 1
CHANNEL	DETAILS						
Name	Max Q	Max V	Chainage	Max	Due to Sto	rm	
	(cu.m/s)	(m/s)	(m)	HGL (m)			
OVERFLO'	W ROUTE DE	ETAILS					
Name		S Max Q D/S	Sate Q			Max Widtl	n Max V Due to Storm
UFI	U	, t	2.90	9 0) 0	L L) 0
DETENTIC	ON BASIN DE	TAILS					
Name	Max WL	MaxVol	Max Q	Max Q	Max Q		
			Total	Low Level	High Level		
Basin2	11.54	1	0.0	1 0.01	0		
					c // =		
Noda	Inflow	Outflow	25 minutes storm,	average 83.	.o mm/n, 20	пет	
NOUE	(cu m)	(cu m)		%			
N52	9.44	9.44	(ca,	0 0)		
Basin2	10.11	. 10.08	3 0.0	1 0.2	<u>)</u>		
N55	10.08	10.08	3	0 0)		

APPENDIX 5 - CONCEPT STORMWATER PLAN- 09447 DA01



